

Navier-Stokes solved with finite elements in Firedrake

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assumptions

- all examples here are for 2D domains $\Omega \subset \mathbb{R}^2$
- notation: $\mathbf{u}(t, x, y)$ is velocity and $p(t, x, y)$ is pressure
- density $\rho > 0$ is constant
 - fluid is incompressible
- dynamic viscosity $\mu > 0$ is constant
 - constitutive relation: $\sigma = -pI + 2\mu D\mathbf{u}$
- body force set to zero: $\mathbf{f} = \mathbf{0}$

- units:

$$[\mathbf{u}] = \text{m s}^{-1}$$

$$[p] = \text{N m}^{-2}$$

$$[\rho] = \text{kg m}^{-3}$$

$$[\mu] = \text{kg m}^{-1} \text{s}^{-1}$$

the Navier-Stokes model

- the time-dependent, incompressible, constant-viscosity Navier-Stokes equations are:

$$\rho (\mathbf{u}_t + \mathbf{u} \cdot \nabla \mathbf{u}) = \mu \nabla^2 \mathbf{u} - \nabla p \quad \text{conservation of momentum}$$
$$\nabla \cdot \mathbf{u} = 0 \quad \text{incompressibility (c. of mass)}$$

potential flow past a cylinder

- recall from 2 weeks ago that Nick provided formula for the potential flow past a cylinder
- in a **potential flow** the vorticity is zero: $\boldsymbol{\omega} = \nabla \times \mathbf{u} = \mathbf{0}$
- incompressible potential flows satisfy:

$$\begin{array}{ll} \nabla \times \mathbf{u} = 0 & \text{conservation of momentum} \\ \nabla \cdot \mathbf{u} = 0 & \text{incompressibility (c. of mass)} \end{array}$$

- zero curl ($\nabla \times \mathbf{u} = 0$) so there exists a potential $\mathbf{u} = \nabla \phi$
- ... and by incompressibility ϕ is harmonic: $\nabla^2 \phi = 0$
- assume far field velocity $\mathbf{u} = (U_0, 0)$
- assume non-penetration and free slip on circle $r = a$
- get by separation of variables:

$$\phi(r, \theta) = U_0 \left(r + \frac{a^2}{r} \right) \cos(\theta)$$

potential flow past a cylinder

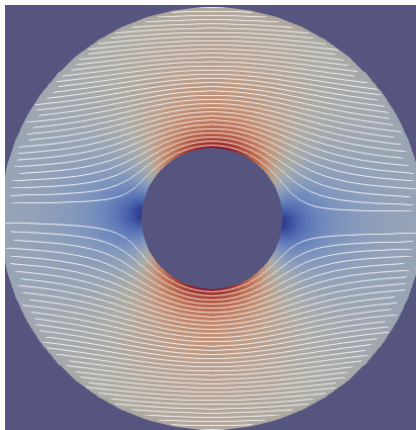
- potential:

$$\phi(r, \theta) = U_0 \left(r + \frac{a^2}{r} \right) \cos \theta$$

- velocity $\mathbf{u} = \nabla\phi$:

$$\mathbf{u}(r, \theta) = U_0 \left(1 - \frac{a^2}{r^2} \right) \cos \theta \hat{\mathbf{r}} - U_0 \left(1 + \frac{a^2}{r^2} \right) \sin \theta \hat{\boldsymbol{\theta}}$$

- *however*, the boundary condition along the cylinder, non-penetration and free slip, is not realistic for a viscous fluid
- in fact there is substantial vorticity along the cylinder
- and flow separation . . .

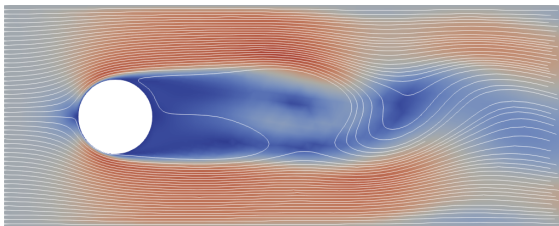
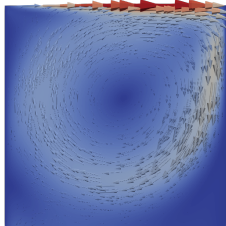


plan for today

- use Firedrake to solve Navier-Stokes (NS) in two situations:

- 1 lid-driven cavity on a square
- 2 flow around a cylinder on a custom mesh

← DEMO NOW!



- TO DO today:

- the Reynolds scaling argument, to reduce # of parameters
- implicit discretization of Navier-Stokes (in time)
- weak form
- practical Firedrake coding
- visualization with Paraview
- meshing with Gmsh

Reynolds number

- recall NS equations:

$$\rho(\mathbf{u}_t + \mathbf{u} \cdot \nabla \mathbf{u}) = \mu \nabla^2 \mathbf{u} - \nabla p, \quad \nabla \cdot \mathbf{u} = 0$$

- a particular simulation sets several scales:

ρ density

μ dynamic viscosity

L (how long and wide is the domain?)

V (how fast is the fluid, e.g. at boundaries?)

- one can change variables in the NS model using these substitutions:

$$\mathbf{u} = V \tilde{\mathbf{u}}, \quad p = \rho V^2 \tilde{p}, \quad \nabla = \frac{1}{L} \tilde{\nabla}, \quad \frac{\partial}{\partial t} = \frac{V}{L} \frac{\partial}{\partial \tilde{t}}$$

- the new variables have tildes: $\mathbf{u}, p, x, t \rightarrow \tilde{\mathbf{u}}, \tilde{p}, \tilde{x}, \tilde{t}$
- the new variables are dimensionless

Reynolds number

- one rewrites the NS equations using the tilde variables . . .
- drop the tildes:

$$\mathbf{u}_t + \mathbf{u} \cdot \nabla \mathbf{u} = \frac{\mu}{\rho V L} \nabla^2 \mathbf{u} - \nabla p, \quad \nabla \cdot \mathbf{u} = 0$$

- note that the coefficient is dimensionless:

$$\frac{[\mu]}{[\rho][V][L]} = \frac{(\text{kg m}^{-1} \text{s}^{-1})}{(\text{kg m}^{-3})(\text{m s}^{-1})(\text{m})} = 1$$

Definition

the *Reynold's number* is the dimensionless ratio

$$\text{Re} = \frac{\rho V L}{\mu}$$

- dimensionless NS equations used from now on ($\text{Re} = \rho VL/\mu > 0$):

$$\mathbf{u}_t + \mathbf{u} \cdot \nabla \mathbf{u} = \frac{1}{\text{Re}} \nabla^2 \mathbf{u} - \nabla p$$
$$\nabla \cdot \mathbf{u} = 0$$

- if Re is small then viscosity is dominant
- if Re is large then inertia is dominant

implicit time steps

- discretization in time typically uses finite differences
- *key idea*: there is no time derivative in the incompressibility equation!
 - thus NS equations are really a “differential-algebraic” system in time, and infinitely stiff, thus implicitness is a good idea
- I will use $O(\Delta t)$ backward (implicit) Euler method, highly stable:

$$\mathbf{u}_t \approx \frac{\mathbf{u}^n - \mathbf{u}^{n-1}}{\Delta t}$$

- suppose \mathbf{u}^{n-1} is known from previous time step, or initial condition
- unknowns are \mathbf{u}^n and p^n :

$$\frac{\mathbf{u}^n - \mathbf{u}^{n-1}}{\Delta t} + \mathbf{u}^n \cdot \nabla \mathbf{u}^n = \frac{1}{\text{Re}} \nabla^2 \mathbf{u}^n - \nabla p^n$$
$$\nabla \cdot \mathbf{u}^n = 0$$

- these equations are continuous in space

implicit time steps

- cleaner notation $\mathbf{u} = \mathbf{u}^n$, $p = p^n$, $\mathbf{u}^{\text{old}} = \mathbf{u}^{n-1}$
- also clear Δt from denominator ... get:

implicit-step Navier-Stokes equations

$$\mathbf{u} - \mathbf{u}^{\text{old}} + \Delta t \left(\mathbf{u} \cdot \nabla \mathbf{u} - \frac{1}{\text{Re}} \nabla^2 \mathbf{u} + \nabla p \right) = 0$$
$$\nabla \cdot \mathbf{u} = 0$$

- we will solve these equations for \mathbf{u} , p **at every time step**, over the domain Ω , using the boundary conditions, and using \mathbf{u}^{old} from the previous time step or the initial conditions

weak form of NS equations

- above equations are the “strong form”, in which \mathbf{u} must have second derivatives and p must have first derivatives
- this is not necessary, and in finite element (FE) method not desirable
- the **weak form** is built by multiplying by test functions and integrating
- multiply 1st equation by \mathbf{v} and 2nd q , and integrate:

$$\int_{\Omega} (\mathbf{u} - \mathbf{u}^{\text{old}}) \cdot \mathbf{v} \, dx + \Delta t \int_{\Omega} \left(\mathbf{u} \cdot \nabla \mathbf{u} - \frac{1}{\text{Re}} \nabla^2 \mathbf{u} + \nabla p \right) \cdot \mathbf{v} \, dx = 0$$
$$\int_{\Omega} (\nabla \cdot \mathbf{u}) q \, dx = 0$$

- integrate by parts to remove 2nd deriv from \mathbf{u} and 1st deriv from p :

$$\begin{aligned} \int_{\Omega} \left(-\frac{1}{\text{Re}} \nabla^2 \mathbf{u} + \nabla p \right) \cdot \mathbf{v} \, dx &= \int_{\Omega} \nabla \cdot \left[-\frac{1}{\text{Re}} (\nabla \mathbf{u}) \mathbf{v} + p \mathbf{v} \right] \, dx - \int_{\Omega} -\frac{1}{\text{Re}} \nabla \mathbf{u} : \nabla \mathbf{v} + p (\nabla \cdot \mathbf{v}) \, dx \\ &= \int_{\Omega} \frac{1}{\text{Re}} \nabla \mathbf{u} : \nabla \mathbf{v} - p (\nabla \cdot \mathbf{v}) \, dx + \underbrace{\int_{\partial \Omega} (p \mathbf{l} - \frac{1}{\text{Re}} \nabla \mathbf{u}) \cdot \hat{\mathbf{n}} \cdot \mathbf{v} \, dS}_{\text{boundary integral}} \end{aligned}$$

boundary conditions

- two boundary conditions considered here, on separate parts of boundary
- **stress free** (Neumann):

$$(\rho l - \frac{1}{\text{Re}} \nabla \mathbf{u}) \hat{\mathbf{n}} = \mathbf{0}$$

- test functions \mathbf{v} unrestricted on this part of boundary
- **given velocity** (Dirichlet):

$$\mathbf{v} \text{ given}$$

- test functions satisfy $\mathbf{v} = \mathbf{0}$ on this part of boundary
- assuming one or the other applies everywhere on boundary, then the boundary integral on last slide is zero

implicit-step Navier-Stokes equations in weak form

$$\int_{\Omega} (\mathbf{u} - \mathbf{u}^{\text{old}}) \cdot \mathbf{v} \, dx + \Delta t \int_{\Omega} \left(\frac{1}{\text{Re}} \nabla \mathbf{u} : \nabla \mathbf{v} + (\mathbf{u} \cdot \nabla \mathbf{u}) \cdot \mathbf{v} - p \nabla \cdot \mathbf{v} \right) dx = 0$$

$$\int_{\Omega} (\nabla \cdot \mathbf{u}) q \, dx = 0$$

for all test velocities \mathbf{v} , with $\mathbf{v} = 0$ on Dirichlet boundary, and for all test pressures q

- the problem is nonlinear in \mathbf{u}
- but the weak form is linear in \mathbf{v} and q
- note: no derivatives on p, q , and only first derivatives on \mathbf{u}, \mathbf{v}

$$\int_{\Omega} (\mathbf{u} - \mathbf{u}^{\text{old}}) \cdot \mathbf{v} \, dx + \Delta t \int_{\Omega} \left(\frac{1}{\text{Re}} \nabla \mathbf{u} : \nabla \mathbf{v} + (\mathbf{u} \cdot \nabla \mathbf{u}) \cdot \mathbf{v} - p \nabla \cdot \mathbf{v} \right) dx = 0$$
$$\int_{\Omega} (\nabla \cdot \mathbf{u}) q \, dx = 0$$

becomes

```
F = dot(u - uold, v) * dx
+ dt * (1.0 / Re) * inner(grad(u), grad(v)) * dx
+ dt * dot(grad(u) * u, v) * dx
- dt * p * div(v) * dx
- div(u) * q * dx
```

solver in Firedrake: lid-driven cavity

```
mesh = UnitSquareMesh(32, 32) # Firedrake utility mesh

V = VectorFunctionSpace(mesh, "CG", 2) # P2 x P1 finite elements
W = FunctionSpace(mesh, "CG", 1)
Z = V * W
up = Function(Z)

u, p = split(up)
v, q = TestFunctions(Z)
F = ... # previous slide

x, y = SpatialCoordinate(mesh)
bcs = [DirichletBC(Z.sub(0), as_vector([4 * x * (1-x), 0.0]), (4,)),
       DirichletBC(Z.sub(0), Constant((0.0, 0.0)), (1, 2)),]

t = 0.0
uold.interpolate(as_vector([0.0, 0.0])) # initial velocity zero
u, p = up.subfunctions
spar = { ... } # for Newton solver
for j in range(N):
    solve(F == 0, up, bcs=bcs, solver_parameters=spar)
    t += dt
    uold.interpolate(u)
```


demonstrations

- Python codes are in `py/bueler/` directory of repository
`github.com/bueler/fluid-solid-seminar`
- you will need to get **Firedrake** installed to use these
- 1 demo: lid-driven cavity on a square
 - look at `navierstokes.py` and `cavity.py`
 - visualize with **Paraview**
- 2 demo: flow around a cylinder on a custom mesh
 - build mesh using **Gmsh**, using geometry-description file `cylinder.geo`
 - look at `navierstokes.py` and `cylinder.py`
 - visualize with **Paraview**
 - play with Reynold's number